within the blast nozzle bar. However, it is also possible to provide, instead of the blast nozzle bores, a continuous slot nozzle in the blast nozzle bar having a slot width of, for example, 1 mm.

As a result of the size of the blast nozzle bar - its length corresponds at least to the strip width and its width is approximately 10 to 500 mm, preferably approximately 60 mm - as well as of the blast nozzle bar surface formed parallel to the strip surface at the side facing the strip, the compressed gas which centrally exits (relative to the width of the blast nozzle bar) from the blast nozzles is able to build up the required air cushion-like compressed gas buffer for a reliable sealing action. Moreover, as a result of the wide configuration of the blast nozzle bar surface at the side facing the strip, whose width projects considerably past the area of the blast nozzle openings and which extends parallel to the strip surface, it is achieved that the gap to be sealed is wide enough in the direction of the strip length in order to maintain, by means of the compressed gas, a reliably acting split flow parallel to the strip surface in the direction toward the rolling mill and in the opposite direction.

Further advantages, details, and features of the invention will be explained in the following with the aid of an embodiment illustrated in the drawing figures.

It is shown in:

Fig. 1 a side view of a detail of the partition and gap sealing at the delivery area of a roll stand (partially in section),

Fig. 2 a schematic enlarged detail of the blast nozzle bar according to Fig. 1.

In Fig. 1, the delivery area of a roll stand (the roll stand has not been illustrated; it is positioned to the right of Fig. 1) with a strip 10 being transported in the direction of arrow 11 is schematically illustrated.

Above and below the strip 10 a stationarily installed partition 12, 13 is provided whose upper part 12 extends up to the stand platform (not illustrated) and whose lower part 13, for the purpose of return of separated liquid, is positioned at a slant downwardly in the direction of the roll stand. The partition 12, 13 opens at the strip into a frame 14, 15 which is also stationarily arranged or is moveably configured and arranged in a movable blast nozzle support 16, 16', 17, 17'. The end of the partition 12, 13 facing the strip provided with the blast nozzle support 16, 16', 17, 17' is formed by blast nozzle bars 18, 19 with centrally arranged blast nozzles 23 in the form of bores which are fastened at the side facing the strip on the blast nozzle supports 16', 17' and which, by means of the movable arrangement of the frames 14, 15 and the movable arrangement of the blast nozzle supports 16, 16', 17, 17', can be moved into a position very close to the strip 10. An adjustable or fixedly installed stop 20 ensures that a certain gap width between the blast nozzle bars 18, 19 and the surface of the strip 10 is adjustable in this connection or is adjusted automatically as a result of the compressed gas buffer, wherein, as a result of the possibility of the movability of the blast nozzle bars, this gap can thus be adjusted also to different strip thicknesses. Together with the components of the blast nozzle supports 16, 16', 17, 17',

the blast nozzle bars 18, 19 form chambers 24, 25, 26, 27, i.e., inner chambers 24, 25 and outer chambers 26, 27 which are in communication with one another via the chamber openings 28, 29. The inner chambers 24, 25 can be filled with the compressed gas via inlet openings 21, 22, and the gas then flows via the chamber openings 28, 29 into the outer chambers 26, 27, and from there it is guided via the blast nozzles 23 perpendicularly onto the surface of the strip 10. As a result of the configuration of the chambers above or below the blast nozzle bar, a reservoir as well as a homogenization for the compressed gas is advantageously provided.

Fig. 2 illustrates the resulting flow directions of the compressed gas, beginning only at the outer chambers 26, 27, in a schematic detail illustration. Even though the components of Fig. 2 are illustrated very schematically and differ in their shape from the components of Fig. 1, the same reference numerals are used for the same components in order to provide a better understanding.

The device according to the invention functions as follows: compressed gas 33 flows from the inner chambers 24, 25 (the chambers are not illustrated in Fig. 2) through the chamber openings 28, 29 into the outer chamber 26, 27 and from there through the blast nozzles 23 perpendicularly onto the surface of the strip 10 and forms here a compressed gas buffer in the gap 30 above and below the strip 10. In the gap 30 the compressed gas 33 is divided and flows in a split flow 32 to the damp area 35 of the roll stand (in Fig. 2 to the right) and in the opposite direction as a split flow 31 to the dry area 34 of the finish-rolled strip (in Fig. 2 to the left). Accordingly, since the blast nozzle bars 18, 19 are formed with a wide blast nozzle bar surface area facing